# HANKEL-MATRIX APPROACH TO INVERTIBILITY OF LINEAR MULTIVARIABLE SYSTEMS 

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The transfer-function matrix $R(s)$ of a linear multivariable system can be represented by the matrix fraction description $R(s)=P(s) Q^{-1}(s)=\tilde{Q}^{-1}(s) \tilde{P}(s)$ or by $R(s)=\bar{P}(s) / q(s)$ where $q(s)$ is the common denominator of all entries in $R(s)$. Based on either of these descriptions, new criteria of $k$-integral invertibility of linear multivariable systems are derived which are expressed as a rank condition of matrices formed by the parameters in the numerator matrix $P(s)$ (or $\tilde{P}(s)$ or $\bar{P}(s)$ ) and denominator matrix $Q(s)$ (or $\tilde{Q}(s)$ or the denominator polynomial $q(s)$ ). A new method based on the Hankel-matrix is used to construct the inverse, to parametrize the set of all minimal order inverses and to identify the stable minimal inverse if one such exists.

## 1. INTRODUCTION

In the last three decades the invertibility of linear systems has been extensively studied with a view to applications in diversified fields of control systems such as coding and decoding problems, filtering and prediction theory, decoupling and synthesis of linear systems, and so on and so forth. Current interest in investigating the fundamental questions of the existence, properties and construction of inverse systems was initiated by Brockett and Mesarović [4] by introducing the concept of functional reproducibility which is a characteristic of right invertible systems. Subsequently Brockett [3] took the help of what is known as left inverse system to offer a state-space interpretation of system zeros. In the following years the invertibility of linear multivariable systems drew the attention of a large number of research workers who were apparently divided principally into three classes. One class of workers (Sain and Massey [15], [18] Dorato [7]) were led by Sain and Massey who brought in the concept of $k$-integral or $k$-delay inverse and stated the invertibility criteria as a rank condition of a matrix of Toeplitz type formed by the system's Markov parameters although state-variable description plays an important
role in their construction of inverse system. Silverman pioneered the second class by presenting his "structure algorithm" ([19], [20]) which could be acclaimed as an important tool for studying the diversified aspects of multivariable systems. An interesting feature of this "structure algorithm" is that it can be applied to the construction of an inverse of time-invariant as well as time-varying multivariable systems starting from their state-variable descriptions. In the third approach (Forney [10]. Hautus [12], Borukhov [2], Wyman and Sain [24]) the system is described by a transfer-function matrix in which the elements are looked upon as elements over a PID $\mathbb{R}\left[\left[s^{-1}\right]\right], \mathbb{R}$ is the field of real numbers or over a PID $Q$ where $Q$ is a ratio of polynomials in $\mathbb{R}[s]$ and invertibility criteria are stated in terms of what is called invariant factors or $\mathscr{F}$-MacMillan form of the transfer-function matrix. Or a theory of inverse system can be laid down with the concept of zero module and pole module.

There are a number of works devoted primarily to the study of stable inversion (Antsaklis [1] and Moylan [16]) or to the study of inverse system of minimal order (Kučera [14], Wang and Davison [22], Forney [11] and Yuan [25]). Sain-Massey criterion of invertibility was improved by tightening the bounds on inherent integrations or delays in (Willsky [23]) and additional criteria of invertibility were given in (Wang and Davison [22]).

In deriving the invertibility criteria in all above cases one has to start with the statespace description $(A, B, C, D)$ of the system or with the manipulation of the elements in transfer-function matrix $R(s)$ which is considered as having elements over the field $\mathbb{R}(s)$ of fractions of the ring $\mathbb{R}[s]$ of polynomials with coefficients from the realnumber field $\mathbb{R}$. By expressing $R(s)$ as $P(s) / q(s)$ where $q(s)$ is common denominator of all the elements in $R(s)$, Orner [17], however, related in a straight-forward fashion the Sain-Massefy invertibility criterion given in terms of Markov parameters to a similar criterion expressed in terms of coefficient matrices $P_{i}$ 's in the polynomial matrix $P(s)$. With the same system description $P(s) / q(s)$ Emre and Hüseyin [9] gave invertibility criteria in terms of $P_{i}$ 's but different from the above.

From a careful scrutiny of the foregoing references it seems justified to set up a procedure for the study of $k$-integral invertibility of linear multivariable systems when they are expressed as a (right or left) matrix fraction description in the form $R(s)=P(s) Q^{-1}(s)=\tilde{Q}^{-1}(s) \widetilde{P}(s)$. The purpose of this paper is, therefore, to establish an invertibility theory based on the matrix fraction description by deriving a new invertibility criterion and a constructive procedure for an inverse system, and making an effort to answer such questions as how to obtain an inverse of minimal order and how to achieve a stable inverse. It is a consequence of the proposed theoretical approach to generate a sufficient number of Markov parameters associated with the inverse system from which its state-space realization is determined in a bid to construct the inverse by applying the existing realization theories. The above invertibility criterion and constructive procedure can be specialized to the case when the transfer-function matrix is expressed as $R(s)=P(s) \mid q(s)$ from which follows Orner's criterion. One can apply the invertibility results established in this paper to discrete-
time system as well although the underlying system with the help of which the foregoing results will be established is a continuous time system.

After a preliminary description in Section 2 of the multivariable system and its inverse with which we shall mainly concern ourselves in this paper, we present the main results in Section 3. The construction of an inverse possibly of a minimal order is described in Section 4.

## 2. SYSTEM DESCRIPTION

Let a linear time-invariant multivariable system $\mathscr{S}$ be described by:

$$
\begin{align*}
\mathscr{S}: \dot{x}(\tau) & =A x(\tau)+B u(\tau)  \tag{2.1a}\\
y(\tau) & =C x(\tau)+D u(\tau), \tag{2.1~b}
\end{align*}
$$

where $u(\tau) \in \mathbb{R}^{m}$ is the input, $x(\tau) \in \mathbb{R}^{n}$ is the state, $y(\tau) \in \mathbb{R}^{r}$ is the output, $A, B, C$ and $D$ are real constant matrices of compatible dimensions. The transfer function matrix $R(s)$ of the system $\mathscr{S}$ is a rational function matrix of order $r \times m$ given by

$$
\begin{equation*}
R(s)=C(s I-A)^{-1} B+D \tag{2.2}
\end{equation*}
$$

which as well can be written as

$$
\begin{equation*}
\overline{\mathscr{S}}: \quad R(s)=P(s) Q^{-1}(s), \tag{2.3}
\end{equation*}
$$

where $P(s)=\left[p_{i j}(s)\right]$ is a polynomial matrix of order $r \times m$ expressed as:

$$
\begin{equation*}
P(s)=P_{0} s^{l}+P_{1} s^{l-1}+\ldots+P_{l} \tag{2.4}
\end{equation*}
$$

$P_{i}$ 's $(i=0,1, \ldots, l)$ being $r \times m$ real constant matrices, $P_{0} \neq 0, l=\max _{i, j}\left[\operatorname{deg} p_{i j}(s)\right]$
and $Q(s)$ is a matrix of order $m$ expressed as and $Q(s)$ is a matrix of order $m$ expressed as

$$
\begin{equation*}
Q(s)=Q_{n} s^{n}+Q_{n-1} s^{n-1}+\ldots+Q_{1} s+Q_{0} \tag{2.5}
\end{equation*}
$$

$Q_{i}$ 's $(i=0,1, \ldots, n)$ being $m \times m$ matrices and $l \leqq n$. At the beginning we shall study the invertibility of $\overline{\mathscr{S}}$ by assuming that $Q_{n}$ is nonsingular.

Now $\hat{R}(s)$, a causal transfer function matrix, is defined to be a $k$-integral (left) inverse of the system $\overline{\mathscr{S}}$ if

$$
\begin{equation*}
\hat{R}(s) R(s)=s^{-k} I_{m}, \tag{2.6}
\end{equation*}
$$

which means that $R(s)$ has rank $m$ over the field of rational functions in $s$. The minimum value of $k$ for which (2.6) is satisfied is called the inherent integrations of the invertible system and is denoted by $k_{0}$. The inverse $\hat{R}(s)$ is expressed as a series in $s^{-1}$ as

$$
\begin{equation*}
\hat{R}(s)=R_{0}+R_{1} s^{-1}+R_{2} s^{-2}+\ldots \tag{2.7}
\end{equation*}
$$

where $R_{i}$ 's $(i=0,1,2, \ldots)$ are $m \times r$ real constant matrices. We now insert (2.3) to
(2.5) and (2.7) into (2.6) to get:
(2.8) $\quad R_{0} P_{0}+\left(R_{0} P_{1}+R_{1} P_{0}\right) s^{-1}+\left(R_{0} P_{2}+R_{1} P_{1}+R_{2} P_{0}\right) s^{-2}+\ldots=$

$$
=\left(Q_{n}+Q_{n-1} s^{-1}+\ldots+Q_{n-1} s^{-1}+\ldots+Q_{0} s^{-n}\right) s^{n-(k+l)}
$$

and observing that $k \geqq n-l$, equating coefficients of various powers of $s^{-1}$ for $i=0,1,2, \ldots$ where $i=k+l-n$ on both sides of the above equation (2.8) we have (2.9)
and
(2.10)

$$
X_{j} A_{j}=\bar{Q}_{j},
$$

where

$$
\begin{align*}
& X_{j}=\left(\begin{array}{llll}
R_{0} & R_{1} & \ldots & R_{j}
\end{array}\right) \text {, }  \tag{2.11}\\
& T_{j}=\left[\begin{array}{cccc}
P_{0} & P_{1} & \ldots & P_{j} \\
& P_{0} & \ldots & P_{j-1} \\
& & & \vdots \\
& & & P_{0}
\end{array}\right], j=0,1, \ldots, l ;  \tag{2.12}\\
& A_{j}=T_{j}, \quad j \leqq l ;  \tag{2.13}\\
& A_{j}=\left[\begin{array}{cccccllll}
P_{0} & P_{1} & P_{2} & \ldots & P_{l} & & & & \\
& P_{0} & P_{1} & \ldots & P_{l-1} & P_{l} & & & \\
& & \ddots & \vdots & & \vdots & & & \\
& & & P_{0} & P_{1} & \ldots & P_{l} & 0 \\
& & & & P_{0} & \ldots & P_{l-1} & P_{l} \\
& & & & & & & \vdots \\
& & & & & & & P_{0}
\end{array}\right], j>l ;
\end{align*}
$$

(2.14)
$\bar{Q}_{j}$ is a matrix of order $1 \times(j+1)$ having ( $m \times m$ ) submatrices as elements and is given by

$$
\bar{Q}_{j}=\left\{\begin{array}{l}
(0, \ldots, 0), \quad 0 \leqq j<i ;  \tag{2.15}\\
\left(0, \ldots, 0, Q_{n}\right), \quad j=i, \\
\vdots \\
\text { th col. ith column } \\
\left.\hat{\uparrow}, \ldots, 0, Q_{n}, Q_{n-1}, \ldots, Q_{n-j+i}\right), \quad j>i
\end{array}\right.
$$

$$
\begin{equation*}
Q_{j}=0, \quad j>n \quad \text { and } \quad j>0 \tag{2.18}
\end{equation*}
$$

Note that columns are counted as $0,1, \ldots, j$.
2.19. Remark. In view of ( 2.8 ) it is interesting to observe that the number of inherent integrations $k_{0}$ is lower bounded by $n-l$, a new insight offered by transferfunction approach.
2.20. Example. Let us consider the transfer function

$$
R(s)=\frac{1}{s^{2}+3 s+2}\left[\begin{array}{cc}
s+1 & s+2 \\
s^{2}+s+3 & 2 s \\
3 s & 0
\end{array}\right]
$$

which when put in the form (2.3) gives us

$$
P_{0}=\left[\begin{array}{ll}
0 & 0 \\
1 & 0 \\
0 & 0
\end{array}\right], \quad P_{1}=\left[\begin{array}{ll}
1 & 1 \\
1 & 2 \\
3 & 0
\end{array}\right], \quad P_{2}=\left[\begin{array}{ll}
1 & 2 \\
3 & 0 \\
0 & 0
\end{array}\right], \quad \begin{aligned}
& Q_{2}=I_{2}, \quad Q_{1}=3 I_{2} \\
& \text { and } \quad Q_{0}=2 I_{2}
\end{aligned}
$$

It is obvious that here $n=2, l=2$ and $i=0$ if $k$ is chosen to be zero. Then

$$
\bar{Q}_{j}=\left[\begin{array}{ll}
Q_{2} & Q_{1}
\end{array}\right], \quad j=1>i=0
$$

and

$$
\bar{Q}_{j}=\left[\begin{array}{lllll}
Q_{2} & Q_{1} & Q_{0} & 0 & 0
\end{array}\right], \quad j=4>i=0
$$

and the set $(2.10)$ is inconsistent because

$$
A_{j} \quad \text { and }\left[\begin{array}{l}
A_{j}  \tag{2.21}\\
\bar{Q}_{j}
\end{array}\right]
$$

have not the same rank. Choosing $k=1$ when also $i=1$ we have

$$
\bar{Q}_{j}=\left[\begin{array}{lllll}
0 & Q_{2} & Q_{1} & Q_{0} & 0
\end{array}\right], \quad j=4>i=1
$$

and the matrices in (2.21) have the same rank. Consequently (2.10) is now a consistent set of equations and when solved gives $R_{i}$ 's which describe the inverse $\hat{R}(s)$ of $R(s)$.
2.22. Remark. We claim that for a consistent system of linear equations described by (2.10) for a suitable choice of $i$ the sequence of $m \times r$ matrices $\left\{R_{0} R_{1} \ldots R_{t}\right\}$ in (2.9) is realizable for some finite value of $t$ (cf. [13], Problem 2) if $r \times m$ matrix $P(s)$ is full column rank. To justify our claim we write (2.10) in an expanded form as

$$
\begin{aligned}
& 2 \\
& \left.=\begin{array}{lllllllll}
0 & \ldots & 0 & Q_{n} & Q_{n-1} & \ldots & Q_{0} & 0 & \ldots
\end{array}\right]
\end{aligned}
$$

If rank $P_{0}=q_{0}<m$, there exist a nonsingular matrix $S_{0}$ such that

$$
P_{00}=P_{0} S_{0}=\left[\bar{P}_{00} \mid 0\right]
$$

where $\bar{P}_{00}$ has $q_{0}$ columns and rank $q_{0}$ and
and

$$
P_{j 0}=P_{j} S_{0}=\left[\begin{array}{ll}
\bar{P}_{j 0} & \widetilde{P}_{j 0}
\end{array}\right], \quad j=1,2, \ldots, l ;
$$

$$
Q_{k 0}=Q_{k} S_{0}=\left[\begin{array}{ll}
\bar{Q}_{k 0} & \tilde{Q}_{k 0}
\end{array}\right], \quad k=0,1, \ldots, n
$$

We now add the last $m-q_{0}$ columns in any block column to the last $m-q_{0}$ columns in the block immediately preceding it in an order starting from the second column block both in $\mathscr{P}$ and $\mathscr{2}$ matrices. Then starting from the first column block we substract last $m-q_{0}$ columns in any column block from the last $m-q_{0}$ columns in the next column block again in an order both in $\mathscr{P}$ and $\mathscr{2}$ matrix after which we get the elements in these matrices as

$$
\left[\bar{P}_{j 0}, \widetilde{P}_{j+1,0}\right], \quad j=0,1, \ldots, l-1, \quad \text { and }\left[\bar{P}_{10} 0\right]
$$

and the last $m-q_{0}$ columns in last column block in $\mathscr{P}$ are zero. If $i=0$ the $(n+i+2)$ nd column block in 2 matrix is nonzero, otherwise it is zero, after one step of these two sequences of operations. Now if

$$
\operatorname{rank}\left[\bar{P}_{00} \widetilde{P}_{10}\right]=q_{1}<m
$$

we can find a constant nonsingular matrix $S_{1}$ such that

$$
P_{01}=\left[\begin{array}{l}
\bar{P}_{00} \\
\tilde{P}_{10}
\end{array}\right] S_{1}=\left[\begin{array}{l}
\bar{P}_{01} \\
0
\end{array}\right],
$$

where $\bar{P}_{01}$ has $q_{1}$ columns and rank $q_{1}$. The above step is then repeated till at the end of $\alpha$ steps we have

$$
\operatorname{rank}\left[\bar{P}_{0, \alpha-1} \widetilde{P}_{1, \alpha-1}\right]=q_{\alpha}=m
$$

where

$$
\alpha \leqq \delta=\operatorname{rank}\left[\begin{array}{cccc}
P_{0} & P_{1} & \ldots & P_{t-1} \\
& P_{0} & \ldots & P_{t-2} \\
& & \cdot & \vdots \\
& & & P_{0}
\end{array}\right]
$$

This result follows with a trivial modification of the method given in [8].
After these $\alpha$ steps, the set of equations (2.23) becomes

where

$$
\beta=n+i \quad \text { if } \quad \alpha \leqq i,
$$

and

$$
\beta=n+\alpha \text { if } \alpha>i,
$$

$N_{0}=\left[\bar{P}_{0, \alpha-1}, \widetilde{P}_{1, \alpha-1}\right]$ has full rank $m, N_{a b}$ 's $(a=0, \ldots, l, b=1, \ldots \alpha)$ have some zero columns and $N_{01} \ldots N_{0 \mathrm{z}}$ have rank less than $m$.
Choosing $j>(\alpha+\beta)$ the set of $(j-\alpha-\beta)$ number of equations in the middle of (2.24) as shown can be written as
(2.25)

$$
\underbrace{\mathscr{R}_{j-\alpha-\beta, \beta+1}}_{\left.\begin{array}{lll:lll}
R_{1} & \ldots & R_{\beta-l} & R_{\beta-l+1} & \ldots & R_{\beta+1} \\
& & & & & \\
R_{2} & \ldots & R_{\beta-l+1} & R_{\beta-l+2} & & R_{\beta+2} \\
\vdots & \ldots & \vdots & \vdots & & \ldots \\
\vdots & & \vdots & \vdots & \\
R_{j-\alpha-\beta} & R_{j-\alpha-l-1} & R_{j-\alpha-l} & & R_{j-\alpha}
\end{array}\right]}\left[\begin{array}{l}
0 \\
\vdots \\
0 \\
N_{l} \\
\vdots \\
N_{0}
\end{array}\right]-\left[\begin{array}{l}
0 \\
\vdots \\
0 \\
\vdots \\
0
\end{array}\right]
$$

which shows as $N_{0}$ has full column rank that the last block column of the Hankef matrix $\mathscr{R}_{j-\alpha-\beta, \beta+1}$ in (2.25) can be expressed as a linear combination of the remaining columns for all values of $j>(\alpha+\beta)$. This implies that rank $\mathscr{R}_{j-\alpha-\beta, \beta}=$
$=\operatorname{rank} \mathscr{R}_{j-\alpha-\beta, \beta+1}$. If we choose $j$ to be the least positive integer such that

$$
\begin{equation*}
m(j-\alpha-\beta) \geqq \beta r \tag{2.26}
\end{equation*}
$$

then obviously

$$
\operatorname{rank} \mathscr{R}_{j-\alpha-\beta+1, \beta}=\operatorname{rank} \mathscr{R}_{j-\alpha-\beta, \beta}
$$

These two rank conditions would imply (cf. [13]) that $\left\{R_{1}, R_{2}, \ldots, R_{t}\right\}$ where $t \leqq(j-\alpha)$ is a realizable sequence for the choice of $j$ given by (2.26).

## 3. CRITERIA OF INVERTIBILITY

With the above introduction we now present our first Theorem which is concerned with a criterion of $k$-integral invertibility of the system $\overline{\mathscr{S}}$.
3.1. Theorem. The linear time-invariant multivariable system (LTIMS) $\overline{\mathscr{P}}$ when $Q_{n}$ in (2.5) is nonsingular has a $k$-integral (left) inverse if and only if for some nonnegative integer $\bar{k} \leqq l$

$$
\begin{align*}
& \operatorname{rank}\left(T_{\bar{k}}\right)-\operatorname{rank}\left(T_{k-1}\right)=m, \quad(\bar{k}=0,1, \ldots, l)  \tag{3.2}\\
& \operatorname{rank}\left(T_{-1}\right):=0
\end{align*}
$$

Proof. To prove the claim we note that the inverse of the polynomial matrix $Q(s)$ represented by (2.5) when $Q_{n}$ is nonsingular can be expressed in the form

$$
\begin{equation*}
L(s)=L_{0} s^{-n}+L_{1} s^{-n-1}+L_{2} s^{-n-2}+\ldots \tag{3.3}
\end{equation*}
$$

where $L_{0}$ is nonsingular and we redefine $P(s)$ in (2.4) to write

$$
\begin{equation*}
P(s)=\bar{P}_{0} s^{n}+\bar{P}_{1} s^{n-1}+\ldots+\bar{P}_{n-1} s+\bar{P}_{n} \tag{3.4}
\end{equation*}
$$

where some higher degree coefficient matrices may be zero. It now follows from (2.2) and (2.3) after substituting (3.3) and (3.4) into (2.3) that

$$
\left[\begin{array}{cccc}
\bar{P}_{0} & \bar{P}_{1} & \ldots & \bar{P}_{j} \\
& \bar{P}_{0} & \ldots & \bar{P}_{j-1} \\
& \cdot & \cdot & . \\
& & & \vdots \\
& & & \bar{P}_{0}
\end{array}\right]\left[\begin{array}{cccc}
L_{0} & L_{1} & \ldots & L_{j} \\
& L_{0} & \ldots & L_{j-1} \\
& & \cdot & . \\
& & & L_{0}
\end{array}\right]=\left[\begin{array}{ccc}
D C B & \ldots & C A^{j-1} B \\
D & \ldots & C A^{j-2} B \\
& \cdot & . \\
& & D
\end{array}\right]=: M_{D_{j}}, j \leqq n
$$

whence, since $L_{0}$ is nonsingular, it is evident that

$$
\operatorname{rank}\left(\bar{T}_{j}\right)=\operatorname{rank}\left(M_{D_{j}}\right), \quad j \leqq n
$$

where $\bar{T}_{j}$ is a matrix of the form (2.12) where $P_{i}$ 's are now replaced by $\bar{P}_{i}$ 's given in (3.4). Moreover rank $T_{j}=\operatorname{rank} \bar{T}_{j+n-l}, j=0,1, \ldots, l$. By interchanging rows and columns one can derive from $M_{D_{j}}$ the matrix $M_{i}$ as defined in [18], from which follows the condition given in (3.2).
3.5. Remark. The least integer $k_{\text {min }}$ of $\bar{k}$ satisfying (3.2) is the minimum value of $i$ for which (2.10) has a solution. Therefore from (2.8) the inherent integrations $k_{0}$ of the invertible system are $k_{0}=k_{\min }+n-l \leqq n$. Moreover $\operatorname{rank}\left(A_{\bar{k}}\right)-$ - $\operatorname{rank}\left(A_{k-1}\right)=m$ for all $k \geqq k_{\min }$ which shows that if a $k_{0}$-integral inverse exists so does an inverse with integrations $k>k_{0}$. The finite sequence $\left\{R_{0}, R_{1}, \ldots, R_{t}\right\}$, $t \leqq(j-\alpha)$ obtained as a solution of (2.10) determines the state-space description $\left\{\bar{A}, \bar{B}, \bar{C}, \bar{D}=R_{0}\right\}$ while for $v>t$, we set $R_{v}:=\bar{C} \bar{A}^{v-1} \bar{B}$ which specifies (2.7) completely with the above state-space description.
3.6. Remark. By making $Q(s)$ column proper in (2.3) and then augmenting the column degrees of $P(s)$ and $Q(s)$ appropriately, $Q_{n}$ in (2.5) can always be made nonsingular. Alternatively to achieve a nonsingular $Q_{n}$ we can write (2.3) in the form $R(s)=P(s) q^{-1}(s)$ where $q(s)=s^{n}+q_{n-1} s^{n-1}+\ldots+q_{0}$. Setting $Q(s)=q(s) I_{m}$ it is obvious that $Q_{n}=I_{m}$ is nonsingular.
From the proof of Theorem (3.1) it follows easily
3.7. Theorem. The LTIMS $\overline{\mathscr{S}}$ with $Q_{n}$ nonsingular has a $k$-integral (left) inverse iff for some nonnegative integer $\bar{k} \leqq n$

$$
\begin{gather*}
\operatorname{rank}\left(\bar{T}_{\bar{k}}\right)-\operatorname{rank}\left(\bar{T}_{\bar{k}-1}\right)=m, \quad \vec{k} \leqq n ;  \tag{3.8}\\
\operatorname{rank}\left(\bar{T}_{-1}\right)=0,
\end{gather*}
$$

and the minimum value of $\bar{k}$ satisfying (3.8) gives inherent integrations of the inverse system.

The invertibility criterion contained in Theorem 3.7 when specialized to $R(s)=$ $=P(s) q^{-1}(s)$ gives Orner [17] criterion. Now in (2.5) if $Q_{n}$ happens to be singular then we have the following theorem which can be easily verified.
3.9. Theorem. The LTIMS when $Q_{n}$ in (2.5) is not necessarily nonsingular and has a $k$-integral (left) inverse iff for some nonnegative integer $\bar{k} \leqq l$

$$
\operatorname{rank}\left[\begin{array}{l}
A_{n+k}  \tag{3.10}\\
Q_{n+k}
\end{array}\right]=\operatorname{rank}\left(A_{n+k}\right)
$$

and the number of inherent integrations is $\bar{k}_{\text {min }}+n-l$ where $\bar{k}_{\min }$ is the minimum value of $\bar{k}$ satisfying (3.10).

Let the transfer-function matrix $R(s)$ of the given system $\mathscr{P}$ be expressed by the (left) matrix fraction representation

$$
\begin{equation*}
\tilde{\mathscr{S}}: \quad R(s)=\tilde{Q}^{-1}(s) \tilde{P}(s) \tag{3.11}
\end{equation*}
$$

where

$$
\begin{aligned}
& \widetilde{P}(s)=\widetilde{P}_{0} s^{l}+\widetilde{P}_{1} s^{l-1}+\ldots+\widetilde{P}_{l}, \\
& \widetilde{Q}(s)=\widetilde{Q}_{\tilde{n}} s^{\tilde{n}}+\widetilde{Q}_{\tilde{n}-1} s^{\bar{n}-1}+\ldots+\widetilde{Q}_{0},
\end{aligned}
$$

and $\widetilde{Q}_{\tilde{n}}$ is nonsingular and let $\widetilde{R}(s)$ be the $k$-integral (right) inverse of $\widetilde{\mathscr{S}}$ defined by

$$
R(s) \tilde{R}(s)=s^{-k} I_{r} .
$$

This implies that $R^{\mathrm{T}}(s)$ must have a $k$-integral (left) inverse where $R(s)$ is given by (3.11). This introduction leads, in a manner similar to the derivation of Theorem 3.1, to the following:
3.12. Theorem. The LTIMS $\widetilde{\mathscr{S}}$ when $\widetilde{Q}_{\tilde{n}}$ is nonsingular has a $k$-integral (right) inverse iff for some nonnegative integer $\bar{k} \leqq \tilde{I}$

$$
\begin{align*}
& \operatorname{rank}\left(\tilde{T}_{k}\right)-\operatorname{rank}\left(\tilde{T}_{k-1}\right)=r,  \tag{3.13}\\
& \operatorname{rank}\left(\tilde{T}_{-1}\right)=0,
\end{align*}
$$

where

$$
\widetilde{T}_{j}=\left[\begin{array}{lllll}
\widetilde{P}_{0} & & & & \\
\widetilde{P}_{1} & \widetilde{P}_{0} & & & \\
\vdots & \vdots & & \ddots & \\
\tilde{P}_{j} & \widetilde{P}_{j-1} & \ldots & \widetilde{P}_{0}
\end{array}\right], j \leqq \tilde{l}
$$

and the number of inherent integrations is $\bar{k}_{\text {min }}+\tilde{n}-\tilde{l}$ where $\bar{k}_{\text {min }}$ is the minimum value of $\bar{k}$ satisfying (3.13).

The assumption that $\widetilde{Q}_{\tilde{n}}$ is nonsingular in the toregoing discussion is not too stringent. In fact $\widetilde{Q}(s)$ can always be made row proper and then appropriately augmenting the row degrees of $\widetilde{Q}(s)$ and $\widetilde{P}(s)$ we can choose $\widetilde{Q}_{\tilde{n}}$ invertible. In case $\widetilde{Q}_{\tilde{n}}$ is singular we can put forward a theorem for (right) invertibility similar to Theorem 3.9.

## 4. CONSTRUCTION OF INVERSES

The inverse of the given system is described by (2.7) where the Markov parameters $R_{0}, R_{1}, \ldots$ are obtained as a solution of (2.10). As noted in Remark 3.10 at most $j-\alpha$ number of $R_{i}$ 's are needed to realize the state-space description of the inverse system. The realization algorithms given in [5], [6] are well suited for this purpose. Moreover the state-space description of the inverse system by employing these algorithms are given in multivariable companion forms. If the solution matrices $R_{i}$ 's of (2.10) contain arbitrary parameters then these parameters can possibly be adjusted to give a Hankel matrix formed by these $R_{i}$ 's which is of minimum rank. The state-space realization corresponding to this Hankel matrix of minimum rank is the state-variable description of the inverse system having minimal order. These concepts will be illustrated by the following Example taken from [17] before finally formulating the theory of a minimal order inverse system.
4.1. Example. Let

$$
R(s)=\frac{1}{s^{2}+3 s+2}\left[\begin{array}{cc}
s+1 & s+2 \\
s+3 & s^{2}+2 s \\
s^{2}+3 s & 0
\end{array}\right]
$$

which when considered to be in the form (2.3) gives us

$$
\begin{gather*}
P_{0}=\left[\begin{array}{ll}
0 & 0 \\
0 & 1 \\
1 & 0
\end{array}\right], \quad P_{1}=\left[\begin{array}{ll}
1 & 1 \\
1 & 2 \\
3 & 0
\end{array}\right], \quad P_{2}=\left[\begin{array}{ll}
1 & 2 \\
3 & 0 \\
0 & 0
\end{array}\right]  \tag{4.2}\\
Q_{2}=I_{2}, \quad Q_{1}=3 I_{2}, \quad Q_{0}=2 I_{2} \tag{4.3}
\end{gather*}
$$

Applying Theorem 3.1 we note that the system is invertible. Also we have $n=2$, $l=2, \bar{k}_{\min }=0, k_{0}=\bar{k}_{\min }+n-l=0$ and that a maximum number of $j-\alpha=5$. $R_{i}$ 's are to be computed for realizing the state space description of the inverse system. We denote $R_{i}$ by

$$
R_{i}=\left[\begin{array}{ccc}
r_{11}^{i} & r_{12}^{i} & r_{13}^{i} \\
r_{21}^{i} & r_{22}^{i} & r_{23}^{i}
\end{array}\right]
$$

and then solve (2.10) successively with $P_{i}$ 's and $Q_{i}$ 's given by (4.2) and (4.3) to get

$$
R_{0}=\left[\begin{array}{lll}
r_{11}^{0} & 0 & 1 \\
r_{21}^{0} & 1 & 0
\end{array}\right]
$$

and

$$
\left[\begin{array}{ll}
R_{1} & R_{2}  \tag{4.4}\\
R_{2} & R_{3}
\end{array}\right]=
$$

$=\left[\begin{array}{ll|lll}r_{11}^{1}, & -r_{11}^{0}, & -r_{11}^{0} & r_{11}^{2}, & -r_{11}^{1}, \\ r_{21}^{1}, & -r_{21}^{0}+1, & -r_{21}^{0}-1 & r_{21}^{2}, & -r_{21}^{1}, \\ r_{11}^{2}, & -r_{11}^{1}, & 2-r_{11}^{1}+3 r_{11}^{0} & r_{11}^{3}, & -r_{11}^{2}, \\ r_{21}^{2}, & -r_{21}^{1}, & -1-r_{11}^{0}+3 r_{21}^{0} \\ \hline\end{array}\right.$
where the parameters $r_{11}^{0}, r_{21}^{0}, r_{11}^{1}$, etc. are arbitrary and can be assigned any value whatsoever to make the rank of (4.4) a minimum. By elementary column transformations (4.4) is found to be equivalent to
in which we select $r_{21}^{0}=1$ and all other unassigned parameters equal to zero for a minimum rank of (4.4). This is an obvious choice, although there are other choices for the rank of (4.4) to be a minimum, one of which we shall see later. With the
above choice of arbitrary parameters in $R_{0}, R_{1}, R_{2}, R_{3}$, we now solve (2.10) for $R_{4}$ an $R_{5}$ assigning zero values to arbitrary parameters to get (see [6])


Fig. 1. Computation of state-space realization of the inverse system. Arrows indicate the rows and columns which are of no consequence in constructing state-space realization because $d_{1}=0, d_{2}=0$.

Following the algorithm and the notation given in [6] we find that controllability indices are $d_{1}=0, d_{2}=0$ and $d_{3}=2$ and the inverse system is of minimal dimension 2 represented by

$$
\bar{A}=\left[\begin{array}{rr}
0 & 1 \\
0 & -3
\end{array}\right], \quad \bar{B}=\left[\begin{array}{lll}
0 & 0 & 0 \\
0 & 0 & 1
\end{array}\right], \quad \bar{C}=\left[\begin{array}{rr}
2 & 0 \\
-4 & -2
\end{array}\right], \quad \bar{D}=R_{0}=\left[\begin{array}{lll}
0 & 0 & 1 \\
1 & 1 & 0
\end{array}\right]
$$

If, however, we assign values different from above to the arbitrary parameters in the solution matrices $R_{i}$ 's, e.g.,

$$
\begin{gathered}
R_{0}=\left[\begin{array}{rrr}
-\frac{2}{3} & 0 & 1 \\
1 & 1 & 0
\end{array}\right], \quad R_{1}=\left[\begin{array}{rrr}
\frac{2}{3} & \frac{2}{3} & \frac{2}{3} \\
\frac{4}{3} & 0 & -2
\end{array}\right], \quad R_{2}=\left[\begin{array}{rrr}
-\frac{2}{3}, & -\frac{2}{3}, & -\frac{2}{3} \\
-\frac{8}{3}, & -\frac{4}{3}, & \frac{2}{3}
\end{array}\right] \\
R_{3}=\left[\begin{array}{lll}
\frac{2}{3} & \frac{2}{8} & \frac{2}{3} \\
4 & \frac{8}{3} & \frac{2}{3}
\end{array}\right]
\end{gathered}
$$

we have Fig. 2


Fig. 2. Computation of an alternative realization for the inverse system.
where $d_{1}=1, d_{2}=1, d_{3}=0$ (see [6] for notation). Observing that

$$
A_{2}^{-1}=\left[\begin{array}{ccc}
1 & 0 & -1 \cdot 5 \\
0 & 1 & 2 \cdot 5 \\
0 & 0 & 1
\end{array}\right]
$$

it now follows from Fig. 2 that state-space description of the inverse of minimal order is

$$
\begin{gathered}
\bar{A}=\left[\begin{array}{r:r}
-2 & -1 \\
\hdashline 1 & 0
\end{array}\right], \quad \bar{B}=\left[\begin{array}{rrr}
1 & 0 & -1 \cdot 5 \\
0 & 0 & 2 \cdot 5
\end{array}\right], \quad \bar{C}=\left[\begin{array}{ll}
\frac{2}{3} & \frac{2}{3} \\
\frac{4}{3} & 0
\end{array}\right] \\
\bar{D}=R_{0}=\left[\begin{array}{rrr}
-\frac{2}{3} & 0 & 1 \\
1 & 1 & 0
\end{array}\right]
\end{gathered}
$$

which has all the poles on the left half of the $s$-plane.
We shall now try to theorise the ideas contained in the above example as how to construct an inverse of a minimal order. The first step to construct an inverse $\hat{R}(s)$ by the proposed method is to determine the Markov parameters $R_{0}, R_{1}, \ldots$, associated with $\hat{R}(s)$ by solving a consistent system of equations of the form

$$
\begin{equation*}
R_{0} N_{0}=M_{0}, R_{1} N_{0}+R_{0} N_{1}=M_{1}, \ldots \tag{4.5}
\end{equation*}
$$

as given by (2.24) which is derived from (2.10) where $N_{0}$ is a matrix of full column rank. We now find nonsigular matrices $U$ and $V$ of order $r$ and $m$ respectively such

$$
U N_{0} V=\left[\begin{array}{c}
I_{m} \\
0
\end{array}\right]
$$

$$
\begin{equation*}
\bar{R}_{i}:=R_{i} U^{-1}, \quad \bar{M}_{j}:=M_{j} V \quad \text { and } \quad \bar{N}_{k}:=U N_{k} V \tag{4.7}
\end{equation*}
$$

for all $i=0,1, \ldots, j=1,2, \ldots, \beta$ and $k=0,1,2, \ldots l$ so that solving (4.5) for $R_{0}, R_{1}, \ldots$ is equivalent to solving the set of equations

$$
\begin{equation*}
\bar{R}_{0} \bar{N}_{0}=\bar{M}_{0}, \bar{R}_{1} \bar{N}_{0}+\bar{R}_{0} \bar{N}_{1}=\bar{M}_{1}, \ldots \tag{4.8}
\end{equation*}
$$

for $\bar{R}_{0}, \bar{R}_{1}, \ldots$ i.e. (2.24) with all elements replaced by those in (4.7) respectively. If the sequence $\left\{R_{0}, R_{1}, \ldots\right\}$ represents the realizable system

$$
\Sigma:\left\{\bar{A}, \bar{B}, \bar{C}, \bar{D}=R_{0}\right\}
$$

so does $\left\{\bar{R}_{0}, \bar{R}_{1}, \ldots\right\}$ represent the system

$$
\Sigma_{u}:\left\{\bar{A}, \bar{B} U^{-1}, \bar{C}, \bar{D} U^{-1}\right\}
$$

Let $\overline{\mathscr{R}}_{a b}$ denote the Hankel matrix formed by the elements $\left\{\bar{R}_{1}, \bar{R}_{2}, \ldots, \bar{R}_{a+b-1}\right\}$ i.e., a Hankel matrix similar to that given in $(2.25)$ with $R_{i}$ 's replaced by $\bar{R}_{i}$ 's.

With the above introduction we can put forward the following two assertions which can be easily verified:
4.9. Theorem. Each element in the sequence $\left\{\bar{R}_{0}, \bar{R}_{1}, \bar{R}_{2}, \ldots\right\}$ obtained as a solution of (4.8) has $(r-m) m$ number of arbitrary parameters occupying columns $m+1, \ldots, r$. Consequently the columns $m+1+k r, \ldots, r+k r$, for $k=0,1,2, \ldots$ $\ldots, b-1$ in the Hankel matrix $\overline{\mathscr{R}}_{a b}$ have all elements arbitrarily assignable.
4.10. Corollary. The Hankel matrix $\mathscr{R}_{a b}$ formed by the matrices in $\left\{R_{1}, R_{2}, \ldots\right.$ $\left.\ldots, R_{a+b-1}\right\}$ which are solutions of (2.10) has $m(r-m)(a+b-1)$ number of arbitrary parameters occupying the columns $i_{1}+k r, i_{2}+k r, \ldots, i_{r-m}+k r$ $(k=0,1, \ldots, b-1)$. The arbitrary parameters in $R_{j}$ are designated by

$$
R_{\zeta}^{j}=\left[\begin{array}{llll}
r_{1 i_{1}}^{j} & r_{1 i_{2}}^{j} & \ldots & r_{1 i_{r-m}}^{j}  \tag{4.11}\\
\vdots & \vdots & & \vdots \\
r_{m i_{1}}^{j} & r_{m i_{2}}^{j} & \ldots & r_{m i_{r-m}}^{j}
\end{array}\right]
$$

where $i_{1}, i_{2}, \ldots, i_{r-m}$ identifies the columns of $R_{j}$.
The above Theorem 4.9 and Corollary 4.10 give information concerning the structure of the Hankel matrix associated with the inverse system $\hat{R}(s)$. This structural information will prove crucial very soon in establishing the construction of a minimal order inverse system. Intuitively it is obvious if all the arbitrary parameters are set equal to zero we would get a fixed value for the rank of $\mathscr{R}_{j-\alpha-\beta, \beta+1}$. This value of rank can possibly be reduced by suitably selecting the so-called arbitrary parameters. This observation gives us:
4.12. Theorem. The minimal rank of the Hankel matrix $\mathscr{R}_{j-\alpha-\beta, \beta+1}$ is bounded
below by

$$
\varrho_{m}=\operatorname{rank} \mathscr{R}_{j-\alpha-\beta, \beta+1} \quad \text { with } \quad R_{\zeta}^{p}=0 \quad(p=0,1, \ldots, j-\alpha)
$$

where $j$ is given by (2.26) and the dimension of a minimal order inverse system is lower-bounded by $\varrho_{m}$.

The bound given in Theorem 4.12 is easy to obtain but is not strong enough. A stronger bound is given below. This will be given first in terms of the matrix $\overline{\mathscr{R}}_{a b}$ with which the mathematical formulation is easily done and the criterion derived very simply.

Taking into account (4.6), (4.8) and (2.24) it is not difficult to write the solution of the sequence $\left\{\bar{R}_{0}, \bar{R}_{1}, \ldots, \bar{R}_{t}, \ldots, \bar{R}_{k}\right\}$ :

$$
\begin{gathered}
\bar{R}_{0}=\left[\bar{M}_{0}, \bar{R}_{\zeta}^{0}\right], \quad \bar{R}_{1}=\left[\bar{M}_{1}-\bar{R}_{0} \bar{N}_{1}, \bar{R}_{\zeta}^{\dagger}\right] \\
\bar{R}_{2}=\left[\bar{M}_{2}-\bar{R}_{0} \bar{N}_{2}-\bar{R}_{1} \bar{N}_{1}, \bar{R}_{\zeta}^{2}\right], \ldots, \bar{R}_{l}=\left[\bar{M}_{l}-\bar{R}_{0} \bar{N}_{l}-\ldots-\bar{R}_{l-1} \bar{N}_{1}, \bar{R}_{\zeta}^{l}\right], \\
\text { and } \\
\bar{R}_{k}=\left[\bar{M}_{k}-\bar{R}_{k-l} \bar{N}_{l} \ldots-\bar{R}_{k-1} \bar{N}_{1}, \bar{R}_{\zeta}^{k}\right], \quad k \geqq l ; \quad \bar{M}_{k}=0, \quad k>\beta ;
\end{gathered}
$$

since $\beta \geqq l$, where the arbitrary parameters are represented by $\bar{R}_{\xi}^{j}$ as in (4.11) but with an overhead bar with each element and $i_{1}=m+1, \ldots, i_{r-m}=r$. Inserting these solutions in $\overline{\mathscr{R}}_{j-\alpha-\beta, \beta+1}$ we have

$$
\overline{\mathscr{R}}_{j-\alpha-\beta, \beta+1}=\left[\begin{array}{lll:l}
\bar{R}_{1} & \ldots & \bar{R}_{\beta}, & -\bar{R}_{\beta+1-l} \bar{N}_{l}-\ldots-\bar{R}_{\beta} \bar{N}_{1}, \\
\bar{R}_{2} & \ldots & \bar{R}_{\zeta+1}^{\beta+1} & -\bar{R}_{\beta+2-l}^{\beta+} \bar{N}_{l}-\ldots-\bar{R}_{\beta+1} \bar{N}_{1}, \\
\bar{R}_{\zeta}^{\beta+2} \\
\vdots & & \vdots & \vdots \\
\bar{R}_{j-\alpha-\beta} & \ldots & \bar{R}_{j-\alpha-1}, & -\bar{R}_{j-\alpha-l} \bar{N}_{l}-\ldots-\bar{R}_{j-\alpha-1} \bar{N}, \bar{R}_{\zeta}^{j-\alpha}
\end{array}\right]
$$

Adding $\beta$ th, $(\beta-1)$ st, $\ldots,(\beta+1-l)$ th block columns post-multiplied respectively by $\bar{N}_{1}, \ldots . \bar{N}_{l}$ to the $(\beta+1)$ st, $\ldots$, 1st block column post-multiplied by $\bar{N}_{1}$ to the second we have
$\overline{\mathscr{R}}_{j-\alpha-\beta, \beta+1} W=$

$$
=\left[\begin{array}{l|ll|l}
\bar{R}_{1} & \bar{M}_{2}-\bar{R}_{0} \bar{N}_{2} & , \bar{R}_{\zeta}^{2} &  \tag{4.13}\\
\bar{R}_{2} & , \bar{R}_{\zeta}^{3} & \\
\vdots & \bar{M}_{3}-\bar{R}_{3}-\bar{R}_{1} \bar{N}_{2} & \vdots & \cdots \\
\overline{\bar{R}}_{j-\alpha-\beta} & \bar{M}_{j-\alpha-\beta+1}-\bar{R}_{0} \bar{N}_{j-\alpha-\beta+1}-\ldots \bar{R}_{j-\alpha-\beta-1} \bar{N}_{2}, \bar{R}_{\zeta}^{j-\alpha-\beta+1} &
\end{array}\right.
$$

$$
\left\lvert\, \begin{array}{|l|ll|l}
\bar{M}_{l-1}-\bar{R}_{0} \bar{N}_{l-1} & , \bar{R}_{\zeta}^{l-1} & \bar{M}_{l}-\bar{R}_{0} \bar{N}_{l} & , \bar{R}_{\zeta}^{l} \\
\bar{M}_{l}-\bar{R}_{0} \bar{N}_{l}-\bar{R}_{1} \bar{N}_{l-1}, \bar{R}_{\zeta}^{l} & \bar{M}_{l+1}-\bar{R}_{1} \bar{N}_{l} & , \bar{R}_{\zeta}^{l+1} \\
\vdots & \vdots & \vdots \\
\bar{M}_{l+j-\alpha-\beta-2}-\bar{R}_{j-\alpha-\beta-2} \bar{N}_{l} & \bar{M}_{l+j-\alpha-\beta-1}-\bar{R}_{j-\alpha-\beta-1} \bar{N}_{l}, & \bar{R}_{\zeta}^{l+j-\alpha-\beta-1} \\
-\bar{R}_{j-\alpha-\beta-1} \bar{N}_{l-1}, \bar{R}_{\zeta}^{l+j-\alpha-\beta-2} & & &
\end{array}\right.
$$

where $W$ is an elementary matrix.

$$
\left[\begin{array}{ll|l}
\bar{M}_{\beta}, & \bar{R}_{\zeta}^{\beta} & 0, R_{\zeta}^{\beta+1} \\
0 & , \bar{R}_{\zeta}^{\beta+1} & 0, R_{\zeta}^{\beta+2} \\
\vdots & \vdots & \vdots \\
0 & , \bar{R}_{\zeta}^{j-\alpha-1} & 0, R_{\zeta}^{j-\alpha}
\end{array}\right]
$$

The following simple Lemma is instrumental in establishing the structure of an inverse system.
4.14. Lemma. Let $G$ be the $2 \times 2$ matrix

$$
G=\left[\begin{array}{ll}
p & a p+b q+c \\
q & d p+f q+q
\end{array}\right]
$$

where $p$ and $q$ are two arbitrary parameters, and $a, b, c, d, g$, and $f$ are variables independent of $p$ and $q$. Define

$$
\varrho:=\min _{p, q} \operatorname{rank} G
$$

Then (a) $\varrho<2$, (b) $\varrho=0$, iff $c=g=0$ simultaneously and (c) $\varrho=1$ iff both $c$ and $g$ are not equal to zero.

The minimum value $\varrho=1$ in the above Lemma is attained when $p$ and $q$ satisfy

$$
d p^{2}+(f-a) p q-b q^{2}+g p-q c=0
$$

which is true for $p=q=0$ or an infinite number of nonzero values of $p$ and $q$.
By repeated application of this Lemma 4.14 to (4.13) reveals that if $\bar{R}_{\zeta}^{p, s}$ $(p=1,2, \ldots, j-\alpha)$ are set equal to zero then $\varrho\left(\bar{R}_{\zeta}^{0}\right)=\operatorname{rank} \bar{R}_{j-\alpha-\beta, \beta+1}$ is a minimum with respect to these arbitrary parameters $\bar{R}_{\zeta}^{1}, \ldots, \bar{R}_{\zeta}^{j-\alpha}$ and is a function of $\bar{R}_{\zeta}^{0}$ only. With respect to the parameters in $\bar{R}_{\zeta}^{0}, \varrho\left(\bar{R}_{\zeta}^{0}\right)$ is now minimized to give us a stronger lower bound for the rank $\overline{\mathscr{R}}_{j-\alpha-\beta, \beta+1}$. Denoting by

$$
\bar{R}_{\zeta}=\left[\bar{R}_{\zeta}^{1}, \bar{R}_{\zeta}^{2}, \ldots, \bar{R}_{\zeta}^{j-\alpha}\right]
$$

and $R_{\zeta}$ by a similar matrix without bar, from the preceding discussion it is easy to state
4.15. Theorem. The rank of the Hankel matrix $\overline{\mathscr{R}}_{j-\alpha-\beta, \beta+1}$ is bounded below by

$$
\varrho_{\min }=\min _{\bar{R}_{5}{ }^{\circ}} \operatorname{rank} \overline{\mathscr{R}}_{j-\alpha-\beta, \beta+1} \quad \text { at } \quad \bar{R}_{\zeta}=0
$$

where minimization is effected with respect to the parameters in $\bar{R}_{\zeta}^{0}$.
Since $\overline{\mathscr{R}}$ is obtained from $\mathscr{R}$ by a nonsingular transformation given in (4.7) we have
4.16. Corollary. The dimension of the minimal order inverse system is bounded below by

$$
\varrho_{\min }=\min _{R_{5}} \operatorname{mank}_{j-\alpha-\beta, \beta+1} \quad \text { at } \quad R_{\zeta}=0
$$

where minimization is effected with respect to the parameters in $R_{\zeta}^{0}$.
We would now like to observe that such minimization would cause no computational problem. It is not hard to see that $\mathscr{R}_{j-\alpha-\beta, \beta+1}$ at $R_{\zeta}=0$ has elements linear
in the parameters of $R_{\zeta}^{0}$ having the form

$$
\begin{equation*}
\beta_{p}=\alpha_{p k 0}+\alpha_{p k 1} r_{p i_{1}}^{0}+\alpha_{p k 2} r_{p i_{2}}^{0}+\ldots+\alpha_{p k r-m} r_{p i r-m}^{0} \tag{4.17}
\end{equation*}
$$

where $\alpha_{p k 0}$ 's are real numbers. The values of the parameters in $R_{\zeta}^{0}$ are sought in such a way that $\beta_{p}=0$ if $\beta_{p}$ contains unknown parameters reducing as many elements as possible in a column of $\mathscr{R}_{j-\alpha-\beta, \beta+1}$ to zero within limits of consistency. There are many solutions for these parameters which are then used in $\mathscr{R}_{j-\alpha-\beta, \beta+1}\left(\right.$ at $\left.R_{\zeta}=0\right)$ for a minimum rank. But however the values of parameters in $R_{\zeta}^{0}$ for a minimal rank of $\mathscr{R}_{j-\alpha-\boldsymbol{\beta , \beta + 1}}$ is not unique. Even nonzero values of $R_{\zeta}$ can give rise to innumerable number of minimal order inverses (see Example 4.1).
4.18. Example. In (4.4) of Example 4.1 to get a lower-bound for the rank we set

$$
r_{11}^{1}=r_{21}^{1}=r_{11}^{2}=r_{21}^{2}=r_{11}^{3}=r_{21}^{3}=0
$$

and for parameters $r_{11}^{o}$ and $r_{21}^{0}$ we solve equations of the form $\beta_{p}=0$ as given in (4.17) if $\beta_{p}$ contains an unknown parameter. This operation gives

$$
r_{11}^{0}=0,-\frac{2}{3},-1 \quad \text { and } \quad r_{21}^{0}=1,-1, \frac{1}{3}, 0
$$

but only the solution $(0,1)$ gives a minimum value of rank for (4.4) as already indicated.

After deciding upon a minimal order inverse by the foregoing method we shall now parametrize all the solutions of such an inverse. This parametrization will be facilitated by the following theorem given in [22].
4.19. Theorem. All minimal order $k$-integral inverses of an invertıble system have the same set of observability indices.

The set of observability indices $d_{1}, d_{2}, \ldots, d_{m}$ of the minimal order inverse obtained in view of Theorem 4.15 will give a corresponding number of independent rows in $\overline{\mathscr{R}}_{j-\alpha-\beta, \beta}$ which can be identified. With the help of these earmarked number of rows, Gaussian elimination procedure is applied either to $\overline{\mathscr{R}}_{j-\alpha-\beta, \beta}$ or to $\overline{\mathscr{R}}_{j-\alpha-\beta, \beta} \bar{W}$ (see (4.13), $\bar{W}$ is $W$ without last $r$ columns) to reduce to zero as many elements as possible on the dependent rows in it. Elements, in the earmarked independent rows, which are real numbers or are in terms of arbitrary parameters in the solution $\bar{R}_{i}$ 's of (4.8) will take part in this reduction process but preference would be given to real number elements. The nonzero elements on the dependent rows are now set equal to zero, the existence of solutions for the arbitrary parameters from these equations being quaranteed by Theorem 4.19. If there are more arbitrary parameters than the number of equations, these excess arbitrary parameters will parametrize all the minimal order inverses. The row operations in the Gaussian elimination process will generate an elementary matrix $Z$ such that $Z \overline{\mathscr{R}}_{j-\alpha-\beta, \beta} \bar{W}$ will contain only $d_{1}+d_{2}+\ldots+d_{m}$ number of independent rows. Following a dual version of the realization algorithm given in [6], $\bar{A}$ in the inverse system $\Sigma$ can be directly obtained from the elements
in last $m$ rows of $Z$. The matrix $\bar{A}$ is therefore given in terms of some arbitrary parameters from which the permissible number of excess parameters will then determine how many eigenvalues of $\bar{A}$ which are consequently poles of $\Sigma$ can be arbitrarily assigned and wiil therefore generate a minimal order stable inverse if one such exists.
4.20. Example. Choosing $r_{j 1}^{i}=x_{2 i+j}, i=0,1,2,3$ and $j=1,2$ the matrix in (4.4a) can be transformed by Gaussian process to

$$
\begin{align*}
& {\left[\begin{array}{ll|ll}
1 & 0 & 0 & 0 \\
1 & 1 & 0 & 0 \\
\hline 2+3 x_{1} / 2 & 1+3 x_{1} / 2 & 1 & 0 \\
\left(1+3 x_{2}\right) / 2\left(-1+3 x_{2}\right) / 2 & 0 & 1
\end{array}\right]\left[\begin{array}{lll|lll}
x_{3}-x_{1} & 0 & x_{5} & 0 & 2 \\
x_{4} & -x_{2}+1 & -2 & x_{6} & 0 & -2 \\
A_{1} & A_{2}
\end{array}\right]=}  \tag{4.21}\\
& =\left[\begin{array}{llr:lrl}
x_{3} & -x_{1} & 0 & x_{5} & 0 & 2 \\
x_{3}+x_{4} & -x_{1}-x_{2}+1 & -2 & x_{5}+x_{6} & 0 & 0 \\
\hdashline 0 & 0 & 0 & 0 & 0 & 0 \\
0 & 0 & 0 & 0 & 0 & 0
\end{array}\right]
\end{align*}
$$

when solutions for

$$
\begin{array}{ll}
x_{1}+x_{3}+\alpha \delta=0, & x_{1}+x_{4}+\alpha \varepsilon=0,  \tag{4.22}\\
x_{3}+x_{5}+\beta \delta=0, & x_{3}+x_{6}+\beta \varepsilon=0, \\
x_{5}+x_{7}+\gamma \delta=0, & x_{5}+x_{8}+\gamma \varepsilon=0,
\end{array}
$$

must exist where

$$
\begin{gathered}
\alpha=x_{1}+x_{2}-1, \quad \beta=x_{3}+x_{4}, \quad \gamma=x_{5}+x_{6}, \quad \delta=1+\frac{3}{2} x_{1}, \\
\varepsilon=\left(-1+3 x_{2}\right) / 2 .
\end{gathered}
$$

The set of six equations (4.22) with eight unknowns gives rise to two excess parameters which can be identified in the following manner. Employing $A_{1}$ and $A_{2}$ in (4.21) the matrix $\bar{A}$ of the inverse $\Sigma$, with the help of a dual version of the algorithm in [6], is

$$
\bar{A}=\left[\begin{array}{rr}
-\left(4+3 x_{1}\right) / 2 & -\left(2+3 x_{1}\right) / 2 \\
-\left(1+3 x_{2}\right) / 2 & \left(1-3 x_{2}\right) / 2
\end{array}\right],
$$

whose characteristic polynomial is

$$
s^{2}+\frac{3}{2}\left(x_{1}+x_{2}+1\right) s+\frac{3}{2}\left(x_{2}-x_{1}-1\right)=0 .
$$

Seeking the poles of the inverse $\Sigma$ to be the solutions of $s^{2}+2 s+1=0$ we determine $x_{1}=-\frac{2}{3}$ and $x_{2}=1$. These values when substituted in (4.22) gives rise to (4.4b) from which a stable inverse follows as already outlined in Example 4.1.

## 5. CONCLUSION

We have shown how an invertibility theory of linear time invariant multivariable systems can be set up based on the matrix fraction description of the system. The inverse system is initially represented by a sequence of Markov parameters from which its state-space description or transfer-function representation can be obtained by using the theory of realization. If one insists on an inverse system of minimal order, it can be achieved by adjusting the arbitrary parameters in the Hankel matrix associated with the inverse system. The same technique can be applied to obtain a stable inverse if one such exists. An interesting question is how minimality and stability of the inverse system can be predicted with some test involving $P_{i}$ 's and $Q_{i}$ 's in (2.4) and (2.5) without solving (2.10) which needs further investigation. The results of this paper can obviously be extended to study the right invertibility of multivariable system invoking the principle of duality.
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## REFERENCES

[1] P. J. Antsaklis: Stable proper $n$th order inverses. IEEE Trans. Automat. Control AC-23 (1978), 1104-1106.
[2] V. T. Borukhov: Invertibility criteria for linear stationary multivariable systems. Avtomat. i Telemeh. (1978), 1, 5-11.
[3] R. W. Brockett: Poles, zeros and feedback: state-space interpretation. IEEE Trans. Automat. Control AC-10 (1965), 129-135.
[4] R. W. Brockett and M. D. Mesarovic: The reproducibility of multivariable systems. J. Math. Anal. Appl. $I I$ (1965), 548-563.
[5] K. B. Datta: Irreducible realization in canonical forms. J. Franklin Inst. 303 (1977), 5, 437-452.
[6] K. B. Datta: Minimal realization in companion forms. J. Franklin Institute 309 (1980), 2, 103-123.
[7] P. Dorato: On the inverse of linear dynamical systems. IEEE Trans. Systems Man Cybernet. SSC-5 (1969), 1, 43-48.
[8] T. Downs, E. Emre and O. Hüseyin: Comments on "On the inversion of rational matrices". IEEE Trans. Circuits and Systems CAS-22 (1975), 4, 375-376.
[9] E. Emre and O. Hüseyin: Invertibility criteria for linear multivariable systems. IEEE Trans. Automat. Control AC-19 (1974), 3, 609-610.
[10] G. D. Forney: Convolutional codes I: Algebraic structure. IEEE Trans. Inform. Theory IT-16 (1970), 6, 720-738.
[11] G. D. Forney: Minimal bases for rational vector spaces, with application to multivariable linear systems. SIAM J. Control 13 (1975), 3, 493-520.
[12] M. L. J. Hautus: The formal Laplace transform for smooth linear systems. In: Mathematical Systems Theory - Proceedings of the International Symposium Udine, Italy, June 16-27, 1975 (G. Marcheseni, S. K. Mitter, eds.). (Lecture Notes in Economics and Mathematical Systems 131.) Springer-Verlag, Berlin-Heidelberg-New York 1976, pp. 29-47.
[13] R. E. Kalman: On minimal partial realizations of a linear input/output map. In: Aspects of Network and System Theory, Holt, Rinehart and Winston 1971, pp. 385-407.
[14] V. Kučera: On the minimal order inverses for linear time-invariant discrete systems. Preprint, JACC, paper no. 5-C 2, (1971), 312-318.
[15] J. L. Massey and M. K. Sain: Inverses of linear sequential circuits. IEEE Trans. Comput. C-I7 (1968), 330-337.
[16] P. J. Moylan: Stable inversion of linear systems. IEEE Trans. Automat. Control AC-22 (1977), 1, 74-78.
[17] P. A. Orner: Construction of inverse systems. IEEE Trans. Automat. Control AC-17 (1972), 1, 151-153.
[18] M. K. Sain and J. L. Massey: Invertibility of linear time-invariant dynamical systems. IEEE Trans. Automat. Control AC-14 (1969), 141-149.
[19] L. M. Silverman: Inversion of multivariable linear systems. IEEE Trans. Automat. Control $A C-14$ (1969), 270-276.
[20] L. M. Silverman and H. J. Payne: Input-output structure of linear systems with application to the decoupling problem. SIAM J. Control 9 (1971), 193-233.
[21] S. H. Wang and E. J. Davison: A minimization algorithm for the design of linear multivariable systems. IEEE Trans. Automat. Control AC-18 (1973), 3, 220-225.
[22] S. H. Wang and E. J. Davison: A new invertibility criteria for linear multivariable systems. IEEE Trans. Automat. Control AC-18 (1973), 538-539.
[23] A. S. Willsky: On the invertibility of linear systems. IEEE Trans. Automat. Control AC-19 (1974), 3, 272-274.
[24] B. F. Wyman and M. K. Sain: The zero module and essential inverse systems. IEEE Trans. Circuits and Systems CAS-28 (1981), 2, 112-126.
[25] Fu-Min Yuan: Minimal dimension inverses of linear sequential circuits. IEEE Trans. Automat. Control AC-20 (1975), 1, 42-52.

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